

# Chapter 5 — Reinforced Concrete

# Section 5-4 — Concrete Design Program (CONC)

## Contents

Introduction	5-4.1
General Description	5-4.4
Input Panel Instructions	5-4.4
General Data Panel	5-4.4
Structure Data Panel	5-4.6
Rebar Data Panel	5-4.7
Service Load Data Panel	5-4.8
Example Problem 1	
Box Girder Design	5-4.10
Computer Output - Design	5-4.11
Example Problem 2	5-4.17
Bent Cap Design	5-4.17
Computer Output – Design	
Input Data Format (Xedit)	5-4.24
General Data	5-4.24
Structure Data	



## Input Data Format (Xedit) - continued

5-4.24
5-4.25
5-4.25
5-4.25
5-4.26
5-4.27



## Concrete Design Program Instructions for Users

## Introduction

This program is available as "CONC" on the Bridge Menu. This program will design or check reinforced concrete (RC), or Fully Prestressed Concrete (FP), or Partially Prestressed Concrete (PP) sections using the "Bridge Design Specifications" of the California Department of Transportation, hereafter referred to as the Code. The cross section may have a rectangular or flanged shape. Up to eight layers of reinforcing steel may be input and will be in either tension or compression depending on the applied loads. The bars may be input as single bars or bundled two vertically or two horizontally. The program determines the area of tension steel required to resist applied dead load and live load moments.

The program uses the STRENGTH DESIGN METHOD (Load Factor Design) based on the assumptions given in article 8.16 of the code, and on the satisfaction of the applicable conditions of equilibrium of internal stresses and compatibility of strains. At the factored level the program considers the standard HS-20 (H-FAC) and CALTRANS Permit (P-FAC) truck loadings as described in article 3.22 of the code.

The program has an option to consider loads at the service level to satisfy the serviceability requirements (Code 8.16.8) for fatigue (F-SER) and crack control (C-SER). For investigation of stresses at the service level, the straight-line theory of stress and strain is used with the assumptions as outlined in article 8.15.3 of the Code.

Input parameters include general control data, material properties, structure dimensions, rebar layout and load data. The program uses panel input (4 panels) and, where practical, parameters are defaulted to commonly used values. The program also has an XEDIT mode which allows the user to by-pass the panels and directly edit the input data file.

The program calculates the area of steel required for fatigue, crack control, factored moment (Mu), 1.2 times the cracking moment, .75 times the balanced steel ratio and prints the controlling load type. To facilitate bar cutoff calculations, the program prints the moment capacity (design moment strength) based on 100%, 80%, 60%, 40%, 20% and 0% of the area of main steel required for the controlling load type.

A table of final results containing the area of steel required for different bar sizes is also printed. The table indicates the controlling load type, maximum service stress, allowable service stress, fatigue stress range, allowable fatigue stress range, effective depth, area of steel, and rebar spacing. The program checks the bar spacing based on the code (8.21.1) and CALTRANS preferred bar spacing.



## Input Panels

TITLE:			
(RC) REINFORCED CONCRETE		10	
(RC) REINFORCED CONCRETE (PP) PARTIALLY PRESTRESSED			
(FP) FULLY PRESTRESSED			
TYPE OF STRUCTURE	(RC/PP/FP)		
TIPE OF SINCLIVES	(Ne/FF/LE)	-	
TYPE OF ANALYSIS (DES	SIGN OR CHECK)	•	
CONSIDER PATIGUE?	(YES/NO)		
CONSIDER SERVICE - CRACK CONTROL?	(YES/NO)		
ULTIMATE CONCRETE COMPRESSIVE STRESS	(PC)	-	K67
ULTIMATE CONCRETE COMPRESSIVE STRAIN	10.44	-	
YOUNG'S MODULUS FOR STEEL REBARS		:	
YIELD STRESS FOR STEEL REBARS		-	
ULTIMATE STRESS FOR PRESTRESS STEEL (	270/250) (FP)	=	KSI
LOW-LAX PRESTRESS STEEL?	(YES/NO)		4
ENVIRONMENTAL FACTOR FOR CRACK CONTRO	L (2)		K/IN
	and the second	THE RESIDEN	(September
STRUCTURE	DATA		
TOTAL DEPTH	*	F	T
TOP FLANGE EFFECTIVE WIDTH	(COMP) =	F	T
TOP FLANGE EFFECTIVE WIDTH			
TOP FLANGE THICKNESS		1	N
		0.2	m -
WIDTH OF WEB		F	•
614 1514 434 1711 18 9 6 1	DTH (COMP) =		8
BOTTOM FLANGE EFFECTIVE WI			r
614 1514 434 1711 18 9 6 1	DTH (TEN) =		r
BOTTOM FLANGE EFFECTIVE WI BOTTOM FLANGE EFFECTIVE WI	DTH (TEN) =		r
BOTTOM FLANGE EFFECTIVE WI BOTTOM FLANGE THICKNESS NOTES	DTH (TEN) =	F	T T
BOTTOM FLANGE EFFECTIVE WI BOTTOM FLANGE THICKNESS	TOTAL DEPTH A	P P	T T N OF WEB ONLY.
BOTTOM FLANGE EFFECTIVE WILL BOTTOM FLANGE THICKNESS  NOTES  1. FOR RECTANGULAR SHAPED BEAMS ENTER	TOTAL DEPTH A	P P	T T N OF WEB ONLY.
BOTTOM FLANGE EFFECTIVE WILL BOTTOM FLANGE EFFECTIVE WILL BOTTOM FLANGE THICKNESS  NOTES  1. FOR RECTANGULAR SHAPED BEAMS ENTER 2. FOR 'T' BEAMS ENTER TOTAL DEPTH, W.	TOTAL DEPTH A	P P P I	T T N OF WEB ONLY. BOTTOM FLANGE

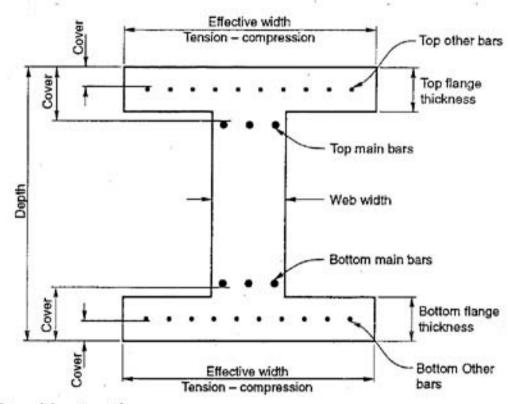


				STEEL	DATA		29	- 6	2.30	
	REBAR		TOTAL	BAR	COVER	BUNDLE	SKEW			
	LOC	LAYER	BARS	SIZE	(IN)	PATTERN	ANGLE			
			=	_	=					
	_		_	_			- 6			
	_	_	_	_		_				
	-	_	_	_		_				
		=	_	_		_				
			_	_						
OTAL AR	EA OF PRE	STRESS	STEEL (	AP) =		o IN				
ISTANCE	FROM BOT	TOM OF	SECTION	TO C.0	. OF PRE	STRESS ST	CEL (DPS) a		IN	
			BON	DLE PAT	TERM:					
				= 1 BA						
			27	= 2 BA	RS VERTI	CAL				
			210	- 2 ma	RS HORIZ	OATTO T.				

		SERVICE	LOAD DATA (K	IP-FT)			
	LOAD TITLE	=					
	TOTAL DEAD LOAD	MAX H-LOAD	MIN H-LOAD	MAX P-LOAD	OTHER	SECONDARY MOMENT	
AXIAL	== :		:			_	
LOAD FACTORS		9 <del>20000</del>		_	_	_	
	REDUCTION PACT STRESS FORCE A		(PHI)	=_	KIPS		
			NOTES		read total or r		
	2. POSITIVE	+) MOMENT C	AUSES TENSION AUSES TENSION D FOR FATIGUE	NOTTON TA N			



## General Description



## Input Panel Instructions

#### General Data Panel

#### Title

Enter a maximum of 40 alphanumeric characters to identify your problem.

#### Type Of Structure

#### Reinforced Concrete (RC)

Strength design method and serviceability criteria as outlined in the code.

#### Fully Prestressed (FP)

Current Caltrans design specifications require zero tension in the concrete under full dead load, but allow some tension ( $6 \times \sqrt{f_c'}$ ) under full service load. The section is still considered uncracked and is designed using gross section properties and traditional equations of mechanics.



## Partially Prestressed (PP)

The trend in current design practice is to partially prestress structures by combining fully stressed tendons with mild steel reinforcement, allow  $4 \times \sqrt{f'_c}$  tension in the concrete under full dead load, and allow the section to crack under full service load and satisfy ultimate strength and serviceability criteria. Partially prestressed members are designed using the same crack width and mild steel fatigue limitations as reinforced concrete. Maximum service stress in the prestress steel, after losses, is limited to 80% of yield stress. For low lax and normal, 7-strand prestressing strand, the yield stress is equal to 90% and 85% of the ultimate stress, respectively.

The allowable range between maximum and minimum tensile stress in the prestress steel caused by live load plus impact at service load, after losses, shall not exceed 22 ksi.

For more detailed information on the design of partial prestressed structures, see "A Design Procedure for Partial Prestressing of Concrete Box-Girder Bridges," by Steve McBride (SASA – 227-8268).

### Type Of Analysis

Enter the type of analysis, DESIGN or CHECK. The default is DESIGN. In both the DESIGN and CHECK mode, the program computes the number of MAIN tension bars required. In CHECK mode, the designer enters the number of MAIN tension bars, the program makes a comparison to the number of MAIN tension bars computed and prints an applicable 'OK' or 'NG'.

The program prints a table of final results containing a stress analysis for crack control and fatigue requirements. In the DESIGN mode the stress analysis is based on the area of steel required for different bar sizes. In the CHECK mode the stress analysis is based on the area of steel and bar size input.

## Consider Fatigue? (Code 8.16.8.3) (Yes/No)

Enter YES to consider fatigue or NO to neglect it. The program will calculate the stress range between maximum tension stress and minimum stress in the steel bars closest to the extreme tension fiber caused by live load plus impact at the service level. An area of steel is determined so that the stress range is equal to the allowable stress range. The default is YES.

Note that fatigue is checked at point of load application. The designer is responsible for assuring fatigue compliance at other sections throughout the span. Generally this is at locations where bars are terminated (cut off).

## Consider Crack Control? (Code 8.16.8.4) (Yes/No)

Enter YES to consider crack control or NO to neglect it. At service level, an area of steel is determined so that the applied stress equals the allowable stress. The allowable stress depends on the number, size and spacing of the bars, the cover from the extreme tension fiber of the concrete to the center of the bar located closest to the extreme tension fiber, the area of concrete in tension having the same centroid as the bar being considered (or the C.G. of a group of bars), and the acceptable crack width (environmental Z factor). The default is YES.



### Ultimate Concrete Compressive Stress

Enter the ultimate concrete compressive strength (ksi). The default is value 3.25 ksi.

### Ultimate Concrete Compressive Strain

Enter the ultimate concrete compressive strain (in/in). The default value is .003 in/in.

### Young's Modulus for Steel Rebars

Enter Young's modulus for the steel rebars (ksi). The default value is 29000 ksi.

#### Yield Stress of Steel Rebar

Enter the yield stress (ksi) of the steel rebar. The default is 60 ksi.

#### Ultimate Stress for Prestress Steel

Enter the ultimate stress for prestress steel. The default is 270 ksi.

#### Low Lax Prestress Steel

Enter yes or no. The yield stress  $(f'_y)$  for low lax strand is calculated as .90 times the ultimate stress  $(f'_y)$ . For normal strand the yield stress  $(f'_y)$  is calculated as .85 times the ultimate stress  $(f'_y)$ .

#### Environmental Factor (Code 8.16.8.4) (Z)

Enter the environmental factor Z(k/in). This is the Z factor used in the crack control check. The default is 170 k/in.

#### Structure Data Panel

#### Total Depth

Enter the total member depth (ft).

#### Top Flange Effective Width (Comp)

Enter the effective width of the flange when the top goes into compression. (Code 8.10)

### Top Flange Effective Width (Ten)

Enter the effective width of the flange when the top goes into tension. (Code 8.17.2)

#### Top Flange Thickness

Enter thickness of top flange (in).



#### Width of Web

Enter width of web (ft.)

## Bottom Flange Effective Width (Comp)

Enter the effective width of the flange when bottom goes into compression. (Code 8.10)

## Bottom Flange Effective Width (Ten)

Enter the effective width of the flange when the bottom goes into tension. (Code 8.17.2)

## **Bottom Flange Thickness**

Enter the thickness of bottom flange (in).

#### Notes:

Since the maximum and minimum applied moments, for the fatigue check, may be opposite in sign, the effective compression and tension flange width for both the top and the bottom of the section is required.

By providing the effective compression and tension flange width for both the top and bottom of the section, the user can design the section for positive moment on one run, then design the section for negative moment on the next run, without having to change the structure data.

For rectangular beams enter the total depth and width of web only.

For 'T-beams' enter total depth, width of web and top or bottom flange data only.

For flanged beams the tension flange width defaults to the compression flange width.

#### Rebar Data Panel

#### Rebar Location

Enter location of the rebar, TOP or BOT. TOP indicates that the rebar cover is measured from the top of the section. BOT indicates that the rebar cover is measured from the bottom of the section.

## Rebar Layer

Enter the type of rebar layer, MAIN or OTHER. The designer must enter at least one MAIN tension rebar layer. MAIN indicates the rebar layer that is to be designed or checked. Only one MAIN rebar layer is allowed at the top and bottom of the section. If the applied moments are positive the area of steel for the bottom MAIN rebar layer will be determined. If the applied moments are negative the area of steel for the top MAIN rebar layer will be determined.

OTHER rebar layers are considered in the design, but their area of steel is held constant. These bars may be in either compression or tension, depending on their location and the applied moment. Up to 6 OTHER rebar layers are allowed.



#### **Total Bars**

Enter total number of bars in the layer. Since the program computes the number of MAIN tension rebars required, the number of rebars in the MAIN tension layer should be left blank in DESIGN mode. If the number of MAIN bars is entered and they go into compression they will be considered as compression steel.

In the CHECK mode the designer must enter the number of rebars in the MAIN tension layer. Always enter the total number of bars in OTHER layers.

#### Bar Size

Enter the Bar size.

#### Cover

Enter the distance from the TOP or BOT of the section to the outside of the rebar (in).

#### **Bundle Pattern**

Enter a '1' for single bars. Enter '2V' for two bars bundled in a vertical pattern. Enter '2H' for two bars bundled in a horizontal pattern.

### Skew Angle

MAIN bars may not be skewed. Only OTHER bars (transverse deck reinforcement) are allowed to be skewed. The program computes an effective steel area by multiplying the actual area of the bars by the cosine of the skew angle. Note by providing both the TOP and BOT MAIN steel, the user can design the section for positive moment on one run, then design the section for negative moment on the next run, without having to change the rebar data.

## Total Area Of Prestressing Steel

Enter the area of prestressing steel (sq in).

## Distance From Bottom Of Section To C.G. Of Prestress Steel

Enter the distance from the bottom of section to center of gravity of the prestressing steel (in).

#### Service Load Data Panel

#### Load Title

Enter a maximum of 40 alphanumeric characters to describe the load.

#### Dead Load Moment (DL)

Enter the moment due to dead load (k-ft).



### H-Load Moment (LL+I)

Enter the maximum and minimum moment due to standard HS-20 truck + impact loading (k-ft).

### P-Load Moment (LL+I)

Enter the maximum moment due to CALTRANS Permit truck + impact loading (k-ft).

For P-Loads on closely spaced girders (PC) used only for superstructures (i.e. box girders), input the P-Load for the number of lanes loaded.

For widely spaced girders (PW) and substructures (i.e. bent cap), input the P-Load as 1.15 times one lane of 'P' load (1.15P) or input 1.15 times one lane of 'P' load plus one lane of 'H' load (1.15P + H), which ever controls.

#### Other Moment

Enter any other moment you want to consider. (k-ft)

### Secondary Moment

Enter prestressing secondary moment. (k-ft)

#### Axial Loads

Enter the corresponding axial loads for DEAD LOAD, H-LOAD, P-LOAD, and OTHER LOAD. (k)

#### Load Factors

Enter the appropriate load factors for DEAD LOAD, H-LOAD, P-LOAD, and OTHER LOAD. The default values are 1.30, 2.17, 1.30, and 1.30 respectively.

### Strength Reduction Factor

Enter strength reduction factor for bending. Default is .90 for reinforced concrete (RC), and .95 for fully prestressed (FP) and partially prestressed (PP) members.

## Final Prestress Force After All Losses

Enter the final prestress force after all losses in kips.

#### Notes

Negative (-) moment causes tension in the top, therefore there must be a MAIN rebar layer at the top of the section.

Positive (+) moment causes tension in the bottom, therefore there must be a MAIN rebar layer at the bottom of the section.

Minimum moment is used for the fatigue analysis.



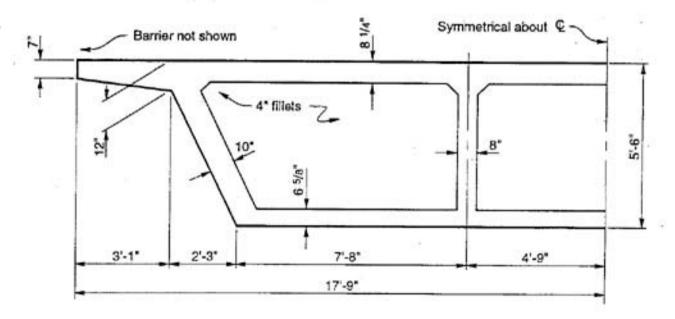
## Example Problem 1

## Box Girder Design

Determine the amount of tension reinforcement required in a box girder for maximum positive moment considering fatigue and crack control criteria.

Service Load Data					
	Dead Load (DL)	H - Load (LL+I)	P - Load (LL+I)		
Max moment	4270	2447	4693		
Min moment		-326	-		

## 1/2 - Typical Section





*********	**********					- 7
YOUR CONC F	ILENAME IS:	BOXGDR				
*********		*********				
BOX GIRDER I	DESIGN			VERSION	2 05.01.87	
RC	DESIGN	YES	YES			
3.25	0.003	29000	60	270	YES	170
5.50						
35.50	33.92	8.25	3.00	24.83	22.63	5.63
1						
Bor	MAIN	0	10	2.06	1	0.00
0.00	0.00		-		-	
MAX POSITIVE	MOMENT					
4270	2447	-326	4693	D	0	
0	0	0	0	0	~	0
1.30	2.17		1.30	1.00	1.00	0.00



```
TITLE BOX GIRDER DESIGN
                                                14:37:52 03/26/93 PAGE 1
                            CONC
                     CONCRETE DESIGN PROGRAM
                     (RC) REINFORCED CONCRETE
                     (PF) PARTIALLY PRESTRESSED
                     (FP) FULLY PRESTRESSED
              CALIFORNIA DEPARTMENT OF TRANSPORTATION
                 VERSION 2 06.01.87
*************
* GENERAL DATA *
TYPE OF STRUCTURE (REINFORCED CONCRETE) = RC
TYPE OF ANALYSIS
                                       = DESIGN
CONSIDER FATIGUE?
CONSIDER SERVICE - CRACK CONTROL? # YES
ULTIMATE CONCRETE COMPRESSIVE STRESS (FC) = 3.25 KSI
ULTIMATE CONCRETE COMPRESSIVE STRAIN (BO) = 0.003 IN/IN
ULTIMATE CONCRETE COMPRESSIVE STRESS (FC) =
                                   (BC) = 3249. KSI
YOUNGS MODULUS FOR CONCRETE
YOUNGS MODULUS FOR STEEL REBARS (ES) = 29000. KSI
YIELD STRESS FOR STEEL REBARS (PS) = 60.0 KSI
YIELD STRESS FOR STEEL REBARS
                                  (PS) »
                                           60.0 KSI
YOUNGS MODULUS FOR PRESTRESS STEEL (EP) = 28000. KSI
ULTIMATE STRESS FOR PRESTRESS STEEL (FP) = 270.0 KSI
LOW-LAX PRESTRESS STEEL
                                       .
MODULAR RATIO MILD STEEL (ES/EC)
                                 (NS) = 8.92
MODULAR RATIO PRESTRESS STEEL (EP/EC) (NP) = 8.62
ENVIRONMENTAL FACTOR
                                   (Z) = 170.0 K/D)
* STRUCTURE DATA *
TOTAL DEPTH
                         ■ 5.50 FT
TOP FLANGE WIDTH (COMP) - # 35.50 FT
TOP FLANGE WIDTH (TEN)
                         - 33.92 FT
TOP FLANCE THICKNESS
                        # 8.25 IN
WIDTH OF WEB
                         = 3.00 FT
BOTTOM FLANGE WIDTH (COMP) = 24.83 FT
BOTTOM FLANGE WIDTH (TEN) # 22.63 FT
BOTTOM FLANGE THICKNESS # 6.63 IN
```



TITLE BOX GIRDER DESIGN

14:37:52 03/26/93 PAGE 2

\*\*\*\*\*\*\*\*\*\*\*\*

· STEEL DATA ·

	REBAR LAYER			COVER (INCH)		SKEW	EPFECTIVE AREA
SOT	MAIN	0	10	2.06	,	0.00	0.00

TOTAL AREA OF FRESTRESS STEEL (AP) = 0.00 SQ IN DIST. FROM SECTION BOTTOM TO C.G. OF PRESTRESS STEEL (DP) = 0.00 IN

· LOAD DATA (KIP-FT) ·

LOAD TITLE - MAX POSITIVE MOMENT

	DEAD LOAD (DL)	H-MAX (LL+I)	H-MIN (LL+I)	F-MAX (LL+I)	OTHER MOMENT (O-MOM)	SECONDARY MOMENT (S-MOM)
MOMENT AXIAL LOAD	4270. 0.	2447. C.	-326. 0.	4693. 0.	0.	٥.
PACTORS	1.30	2.17	22	1.30	1.00	1.00

STRENGTH REDUCTION FACTOR (PHI) = 0.90

FINAL PRESTRESS FORCE AFTER ALL LOSSES (PF) = 0.00 KIPS

\* DESIGN LOADS \*

	MAX	MIN	MAX	MAX
	H-SER	H-SER	H-FAC	P-FAC
MOMENT	6717. 0.	3944.	10861.	11652.

LOAD COMBINATIONS:

MAX H-SER = {DL} + (H-MAX) + (O-MOM) + (S-MOM) MIN H-SER = (DL) + (H-MIN) + (S-MOM)

MAX H-FAC = 1.30 X (DL) + 2.17 X (H-MAX) + 1.00 X (O-MOM) + 1.00 X (S-MOM) MAX P-FAC = 1.30 X (DL) + 1.30 X (P-MAX) + 1.00 X (0-MOM) + 1.00 X (S-MOM)



TITLE BOX GIRDER DESIGN

14:37:52 03/26/93 PAGE 3

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\* INTERMEDIATE RESULTS \*

MAIN STEEL AREA BASED ON FOLLOWING LOAD TYPES:

S-AS = SERVICE STRESS IN MILD STEEL (AS) (MAX H-SER)

(CRACK CONTROL)

F-AS = FATIGUE STRESS IN MILD STEEL (AS) (MAX & MIN H-SER)

H-FAC = H-FACTORED MOMENT

P-PAC = P-FACTORED MOMENT

MIN1 = MINIMUM REINFORCEMENT (8.17.1.1)

BASED ON 1.2 X THE CRACKING MOMENT

MIN2 = WAIVER OF MINIMUM REINFORCEMENT (8.17.1.2)

BASED ON STEEL AREA ONE THIRD GREATER THAN REQUIRED BY ANALYSIS.

MAX = MAXIMUM REINFORCEMENT (8.16.3.1)

BASED ON .75 X BALANCED STEEL RATIO.

EFFECTIVE DEPTH = 63.22 IN

YNA . DISTANCE FROM EXTREME COMPRESSIVE FIBER TO NEUTRAL AXIS.

BAR	LOAD	EAR SPACING (IN)	YNA (IN)	APPLIED MOMENT (K-PT)	MAIN STEEL REQUIRED (SO IN)	HAIN BARS REQ
10	S-AS	8.59	9.59	6717.	40.23	32
10	F-AS	9.87			34.39	28
10	H-FAC	8.88	2.33	10861.	38.78	31
10	P-FAC	8.32	2.50	11652.	41.66	33
10	MINI	19.03	1.07	5025.	17.79	15
10	MIN2	6.19	3.33	15449.	55.55	44
10	MAX	2.26	9.04	40252.	150.64	119
• • • • •	CONTROL					*****
10	P-FAC	0.32	2.50	11652.	41.66	33

ULTIMATE MOMENT CAPACITY.

TOTAL COMP AREA (SQ IN)	TOTAL TEN AREA (SQ IN)	OTHER TEN AREA (SQ IN)	MAIN TEN AREA (SQ IN)	ULT TENDON STRESS (KSI)	MOMENT CAPACITY (K-FT)	YNA (IN)
0.00	41.91	0.00	41.91	0.0	11721.	2.51
0.00	33.53	0.00	33.53	0.0	9409.	2.01.
0.00	25.15	0.00	25.15	0.0	7081.	1.51
0.00	16.76	0.00	16.76	0.0	4737.	1.01
0.00	8.38	0.00	8.38	0.0	2377.	0.50



TITLE BOX GIRDER DESIGN

14:37:52 03/26/93 PAGE 4

· SECTION PROPERTIES AND CONCRETE STRESSES ·

- SECTION PROPERTIES AND CONCRETE STRESSES \*

(APTER ALL LOSSES)

SECTION PROPERTES

MAIN STEEL AREA = 41.91 IN\*\*2

		GROSS	UNCRACKED TRANSPORMED	CRACKED TRANSFORMED	
AREA	(FT*+2)	49.7	52.0	27.4	
INERTIA	(FT**4)	223.9	244.5	57.9	
YOG	(IN)	26.5	28.1	9.8	
YNA	(IN)	26.5	28.1	9.8	

### CONCRETE STRESSES (PSI)

12	UNCRACKED GROSS :		UNCRACKED TRANSFORMED		CRACKED TRANSPORMED :	
LOAD TYPE	TOP	BOTTOM	TOP	BOTTOM	TOP	BOTTOM
MIN H-SER MAX H-SER		403. 686.	-263. -447.	354. 602.	-386. -658.	0.

CONCRETE MODULUS OF KUPTURE

(7.5 X SQRT PC) = 428. PSI

#### NOTES:

YCG = DISTANCE FROM EXTREME COMPRESSION PIBER TO CENTER OF GRAVITY.

YMA . DISTANCE FROM EXTREME COMPRESSION FIBER TO NUETRAL AXIS.

(+) = TENSION

(-) = COMPRESSION



TITLE BOX GIRDER DESIGN 14:37:52 03/26/93 PAGE 5 FINAL RESULTS - DESIGN • \* (AREA OF STEEL REQUIRED FOR DIFFERENT BAR SIZES) :-SERVICE-:-FATIGUE-: BAR LOAD MAX ALLOW STRESS ALLOW EFP BAR REQ TOTAL SPACE SIZE CONT STRESS STRESS RANGE RANGE DEPTH SPACE STEEL BARS CODE (KSI) (KSI) (KSI) (KSI) (IN) (IN) (SQ IN) REQ 18 S-AS 22.67 24.00 9.37 19.01 62.69 18.95 56.61 15 14 S-AS 27.26 28.12 11.26 18.12 63.00 12.66 48.48 11 S-AS 30.78 31.35 12.71 17.44 63.12 9.86 43.18 28 10 P-PAC 32.01 33.86 13.22 17.20 63.22 8.32 41.66 33 9 P-PAC 31.90 36.00 13.17 17.22 63.31 6.50 41.60 42 F-FAC 31.96 36.00 13.19 17.21 63.37 5.13 41.55 7 P-FAC 31.83 36.00 13.14 17.23 63.44 3.87 41.51 70 6 P-FAC 31.95 36.00 13.19 17.21 63.50 2.84 41.47 95 SPACE CODES: 1 = BAR SPACING LESS THAN THE AASHTO MINIMUM. (8.21) 2 = BAR SPACING LESS THAN THE PREFERRED CALTRANS MINIMUM. (BR. DES. DET.)

3 = BAR SPACING MORE THAN THE AASHTO MAXIMUM (18.20)

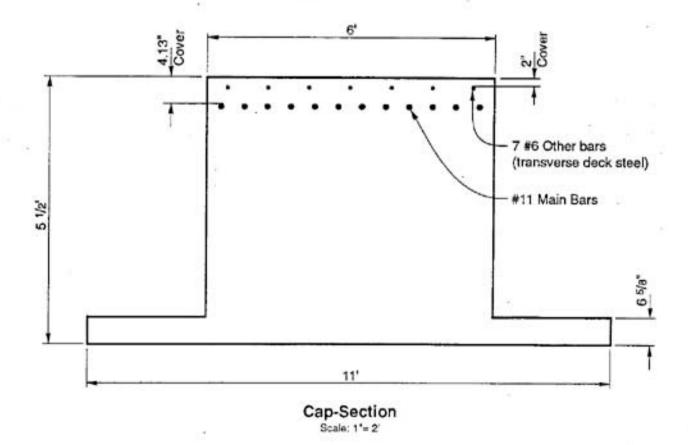


## Example Problem 2

## Bent Cap Design

Determine the amount of tension reinforcement required in a bent cap for maximum negative moment considering fatigue and crack control criteria.

	Service Lo	oad Data	
	Dead Load (DL)	H - Load (LL+I)	P - Load (LL+I)
Max moment	-2146	-706	-2155
Min moment	a same and	0	





CAP DES	IGN WITH	TRANSVER	SE DECT	STEEL	VE	RSION 2	06.01.8
RC	DESIGN	YES	YES				
3.25	0.003	29000	60	270	YES	170	
5.50							
11.00	6.00	8.25	6.00	11.00	6.00	6.63	
2							
TOP	MAIN	0		4.13	1	0.00	
TOP	OTHER	7	6	2.00	1	0.00	
0.00	0.00						
MAXIMUM	NEGATIVE	MOMENT					
-2145	-706	0	-2155	0			
0	0	0	0	0		0	
1.30	2.17	1.30	1.00	1.00		0.90	